Properties of Fired Clay Bricks Mixed with Waste Glass

خصائص الطوب الطيني الحراري بعد خلطه مع مخلفات الزجاج

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نتائج الحكم على أطروحة ماجستير

بناءً على موافقة شئون البحث العلمي والدراسات العليا بالجامعة الإسلامية بغزة على تشكيل لجنة الحكم على أطروحة الباحث/ هشام حسين عابدين عابدين لنيل درجة الماجستير في كلية الهندسة قسم الهندسة المدنية – تصميم وتأهيل المنشآت وموضوعها:

خصائص الطوب الطيني الحراري بعد خلطه مع مخلفات الزجاج

Properties of Fired Clay Bricks Mixed with Waste Class

وبعد المناقشة التي تمت اليوم الأربعاء 22 شوال 1437ه، الموافق 2016/07/27م الساعة الثانية عشرة ظهراً،
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وإن ينصح هذا الج研究成果 ينصحه بإلتقاط الله ولزوم طاعته وأن يشكر علمائه في خدمة دينه ووطنه.

والفتيق...،

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Abstract

The concrete hollow blocks have traditionally been used as construction materials in Gaza Strip, giving people the wherewithal to construct buildings and keep themselves safe. Nowadays, with the Israeli siege that stopped cement from entering into Gaza Strip, fired clay bricks may be used as an alternative to concrete blocks.

The production of fired clay bricks with the incorporation of wastes constitutes a positive way for the brick industry to contribute to a more sustainable construction materials. The advantages are on one hand, a reduction of the clay extraction and, on the other minimization of wastes in landfills.

The main idea of this research is to focus on the ability of making fired clay bricks as alternative masonry units to concrete hollow blocks and enhancing their properties by adding waste glass.

The physical and mechanical properties of fired clay bricks. Also, the effect of waste glass particle size on the properties of the fired clay brick was studied.

The results showed that the firing shrinkage, bulk density, and compressive strength of the bricks increased as the amount of waste glass content increased and firing temperature increased. The apparent porosity and water absorption had the same pattern and they decreased with the increase of the amount of waste glass content and firing temperature.

The results also showed that the particle size of waste glass powder was very important and had a significant effect on the properties of fired clay brick; the finest the particle size, the highest the compressive strength.

The optimal properties of fired brick were found at 30% content of waste glass and firing temperature at 1100°C. The results also implied that it is possible to make bricks with compressive strength of 96.37 MPa and water absorption of 5.93%.

Finally, based on the results of this study, use of waste glass as a brick additive is recommended.

**Keywords:** fired clay bricks, waste glass, recycling, firing temperature, physical and mechanical properties.
الملخص

يعتبر البلوك الخرساني وحدة البناء التقليدية في قطاع غزة، حيث يستخدم في تشييد المباني و إيواء الناس بشكل آمن. لكن في الوقت الحاضر وبسبب الحصار الإسرائيلي الذي يمنع دخول الأسمنت إلى قطاع غزة، الممكن أن يكون الطوب الطيني الحراري بديل عن البلوك الخرساني. ان تناج الطوب الطيني الحراري بعد دمجه مع النفايات يعتبر طريقة إيجابية لصناعته الطوب والمساهمة في جعل موارد البناء أكثر استمرارية، حيث يتم تقلص كمية الطين المستخدم، ومن جانب آخر تقليل رمي النفايات في المكبات.

الفكرة الرئيسية في هذا البحث هي التحقق من امكانية عمل الطوب الطيني الحراري في قطاع غزة، وتحسين خصائصه عن طريق اضافة مخلفات الزجاج.

تم دراسة الخصائص الفيزيائية والميكانيكية للطوب المنتج. كما تم دراسة تأثير حجم حبيبات مخلفات الزجاج على خصائص الطوب.

أظهرت النتائج تحسن جميع خصائص الطوب الطيني الحراري سابقة الذكر مع زيادة محتوى بودرة الزجاج وزيادة درجة حرارة الحرق، كما أن حجم حبيبات مخلفات الزجاج كان له تأثير مهم على خصائص الطوب، حيث أظهرت النتائج أن استخدام حجم حبيبات اصغر هو الأفضل بالنسبة لمقاومة الطوب للكسر.

الخصائص المثالية للطوب الطيني الحراري ظهرت عند اضافة بودرة الزجاج إلى الطين بنسبة 30%， وعند حرق العينة عند درجة حرارة 1100 درجة مئوية، حيث أظهرت النتائج أنه يمكن صناعة طوب يتحمل ضغط مقداره 9.37.37 ميجا باسكال ونسبة امتصاص للماء مقدارها 5.93%.

في الختام ينصح من خلال النتائج استخدام مخلفات الزجاج كضامن للطين عند صناعة الطوب الطيني الحراري لتحسين خواصه.

كلمات مفتاحية: الطوب الطيني الحراري، مخلفات الزجاج، إعادة تدوير، درجة حرارة العرق، الخصائص الفيزيائية والميكانيكية.
Dedication

I would like to dedicate this work to my family particularly my mother and father who loved and raised me and to my loving wife, daughter, sons and to my brothers and sisters, for their sacrifice and endless support.
Acknowledgment

I would like to express my sincere appreciation to prof. Samir Shihada from the Department of Civil Engineering at The Islamic University of Gaza for his help, guidance and assistance in all stages of this research. The constant encouragement, support and inspiration he offered me were fundamental to the completion of this research.

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<tbody>
<tr>
<td>FCB</td>
<td>Fired Clay Brick</td>
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<tr>
<td>WG</td>
<td>Waste Glass</td>
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<tr>
<td>C</td>
<td>Clay</td>
</tr>
<tr>
<td>G</td>
<td>Glass</td>
</tr>
<tr>
<td>IOF</td>
<td>Israeli Occupation Forces</td>
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<tr>
<td>FS</td>
<td>Firing Shrinkage</td>
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<tr>
<td>BD</td>
<td>Bulk Density</td>
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<td>AP</td>
<td>Apparent Porosity</td>
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<tr>
<td>WA</td>
<td>Water Absorption</td>
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<tr>
<td>CS</td>
<td>Compressive Strength</td>
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<tr>
<td>FA</td>
<td>Fluxing Agent</td>
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<tr>
<td>ASTM</td>
<td>American Society for Testing and Material</td>
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<tr>
<td>µm</td>
<td>Micrometer</td>
</tr>
<tr>
<td>MPa</td>
<td>Mega Pascal</td>
</tr>
<tr>
<td>TFT-LCD</td>
<td>Thin Film Transistor-Liquid Crystal Display</td>
</tr>
<tr>
<td>SW</td>
<td>Severe Weathering</td>
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<tr>
<td>FT</td>
<td>Firing Temperature</td>
</tr>
<tr>
<td>TV</td>
<td>Television</td>
</tr>
<tr>
<td>PC</td>
<td>Personal Computer</td>
</tr>
<tr>
<td>CB</td>
<td>Concrete Block</td>
</tr>
<tr>
<td>US</td>
<td>United States of America</td>
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<tr>
<td>UK</td>
<td>United Kingdom</td>
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<tr>
<td>BC</td>
<td>Before Christ</td>
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<tr>
<td>AD</td>
<td>Anno Domini</td>
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<tr>
<td>CNS</td>
<td>Chinese National Standard</td>
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<tr>
<td>SEM</td>
<td>Scanning Electron Microscope</td>
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<tr>
<td>(F/T)</td>
<td>Freeze-Thaw Testing</td>
</tr>
<tr>
<td>C/B</td>
<td>Absorption Coefficient</td>
</tr>
<tr>
<td>USEPA</td>
<td>United States Environmental Protection Agency</td>
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<tr>
<td>ILO</td>
<td>The International Labor Office</td>
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<tr>
<td>UNIDO</td>
<td>The United Nations Industrial Development Organization</td>
</tr>
<tr>
<td>SIDA</td>
<td>Swedish International Development Authority</td>
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Chapter (1)

Introduction
Chapter (1)

Introduction

1.1 Overview

Masonry unit is a significant basic material of construction required in all spheres of constructional activities and constitute about 13 percent of the total cost of building material required for construction (Alam, 2015). Masonry units are bonded together with mortar to yield a composite building component generally a wall. Concrete block and brick are the most common types of masonry units. These construction materials are extensively employed worldwide both in developed and developing countries. In Gaza Strip, concrete blocks which are made from a mixture of Portland cement and aggregates is a main construction element used to make masonry walls, may be due to long time tradition or even the good performance of masonries such as strength properties.

However the production of concrete block became difficult in Gaza Strip. This is due to the Israeli siege that restricts the importation of construction materials such as Portland cement which used to make these masonry units. And also, because of high Portland cement consumption in the concrete. For these reasons, fired clay brick may be used as an alternative masonry unit to concrete blocks in Gaza Strip. It is expected that in the future, this material will gain a higher market share in Gaza Strip.

Worldwide, bricks are a major building material and perhaps one of the oldest. The worldwide annual production of bricks is currently about 1391 billion units and the demand for bricks is predicted to be continuously increasing (Zhang, 2013). In this respect, for the development of bricks with waste materials, further research and development is necessary. Besides, not only on the technical, economic and environmental features but also public education related to waste reusing and sustainable development is required for wide production and application of these bricks.

Clay materials are mostly used for the manufacture of bricks. waste can be added in order to enhance its properties. Solid waste is a great concern among governmental
agencies, and environmentalist regarding the increasing amount of waste throughout the world.

One waste material which has potential as a brick additive is waste glass. It is not biodegradable and therefore creates a problem for solid waste disposal. The disposal into landfills also does not provide an environment-friendly solution. Hence, the use of waste glass in construction materials can be a worthy solution to the environmental problem caused by this solid waste.

United Nations estimates the volume of solid waste disposed of annually over the world to be 200 million tons, 7% of which is made up of glass (Topcu & Canbaz, 2004). For Palestine, this amount approaches 1.2 million tons (PCBS, 2011), 4% of which is made up of glass with no recycling activities exist (ARIJ, 2009).

1.2 Problem Statement

For a long time and still nowadays, concrete blocks which are made from Portland cement, sand and gravel, are main construction elements that are used to make masonry walls in Gaza Strip. Since 2007, Israeli Occupation Forces (IOF) has imposed siege on Gaza Strip and restricted entry of many goods and construction materials such as cement and aggregate. Because of this Israeli ban, this research is to focus on the using of the fired clay bricks as an alternative to concrete blocks.

The second problem in Gaza Strip is the accumulation of solid waste in landfills without any treatment processes. Also, the landfills in Gaza Strip are very limited in both their current and future count number and their individual capacity and efficiency of usage (Work Team Ocha, 2009). This problem was considerably increased and extremely highlighted especially after the repeated Israeli aggression on Gaza Strip in 2008, 2012, and 2014; these resulted in huge amounts of industrial and constructional wastes.

The target for engineers must be developing new ways to recover solid waste into new products by the so called 3R system, reuse, reduce and recycling.

The main idea of this research is to focus on the ability of making fired clay bricks as alternative masonry units to concrete blocks. And enhancing their properties by adding waste glass. Also, the effect of waste glass particle size on the properties of
the fired body is studied. Generally, these wastes create disposal problems as well as environmental pollution on a large scale throughout the world.

1.3 Research Objectives

The main objective of this research is to focus on the ability of making fired clay bricks as alternative masonry units to concrete blocks and to investigate the effect of the addition of waste glass on the properties of the fired clay bricks. These include firing shrinkage, bulk density, apparent porosity, water absorption and compressive strength. Also, the effect of waste glass particle size on the properties of the fired body is studied.

Different amounts of waste glass (0, 10, 20, 30 and 40%) were added to the original brick clay and fired at temperatures of 900, 1000 and 1100°C.

The successful use of waste glass will aid in reducing the environmental and health problems related to the disposal of waste glass and the scarcity of land area needed for disposal.

Reducing waste is not the only reason to investigate the addition of certain residues into a clay matrix, although traditionally it has been the main purpose of research on this topic. Other reasons may be considered. Wastes may save energy required in the manufacturing process and reduce the manufacturing cost. The main aim was achieved through the following objectives:

1. Identify the properties of clay raw materials such as sieve analysis, plastic limit, liquid limit and Plasticity Index.
2. Identify the effects of adding waste glass material on the properties of fired clay bricks mixes such as, firing shrinkage, bulk density, water absorption, apparent porosity, and compressive strength.
3. Determine the optimal waste glass content to be added as a partial replacement of clay.
4. Determine the optimal firing temperatures.
5. Comparison between the properties of bricks when using different waste glass particle size.
1.4 Methodology

The following tasks were done to achieve the research objective:

1. Collecting the required information and documents related to the waste materials such as clay and waste glass.
2. Undertake a comprehensive literature review on relevant subjects focused on the using of waste glass in construction field.
3. Visiting the Gaza city glass shops to obtain related information and collect samples.
4. Develop a suitable experimental program to study the use of waste glass in fired clay bricks.
5. Analyzing the experimental test results to draw conclusions.
6. Conclusions and recommendations.

1.5 Thesis Layout

The present work contains five chapters organized as follows:

Chapter-1 (Introduction)
Introduces the use of the fired clay brick as a masonry building unit. Also, it includes a description of research importance, scope, objectives, methodology, and the report organization.

Chapter-2 (Literature Review)
Presents a general literature review for studying the use of additives such as waste glass to fired clay brick in engineering practice. Also, an overview, history, manufacturing, and types of the fired clay brick and glass was also provided.

Chapter-3 (Experimental Program)
Presents the experimentation program and the used materials. Furthermore, the variables, preparation of raw material, producing and testing of specimens and materials are also illustrated. This chapter ends with details of the testing methods.
Chapter-4 (Test Results and discussion)

Aims to find the properties of fired clay brick such as compressive strength, firing shrinkage, water absorption, apparent porosity, bulk densities and the methodology followed to highlight the usefulness of adding of recycled waste glass material as an additive to fired clay bricks to improve their properties.

Chapter-5 (Conclusions and Recommendations)

A comprehensive summary of this research study, its major conclusions, and recommendations for future research are presented.

References.

It includes the listing of references used in preparing the study.

Appendices.

It includes Tables from the ASTM Standard and divided into "A".
Chapter (2)

Literature Review
Chapter (2)

Literature Review

2.1 Background

Bricks have been widely used as construction and building material all around the world for a long time. Conventional clay based brick production generally uses the mixtures of clays as raw materials, and requires the processes of shaping, drying and firing at a high temperature. Fired clay bricks are the best known type of brick construction materials as a masonry wall, both in loadbearing and non-load-bearing walls. The use of fired clay bricks masonry walls is mostly used in the construction of non-load-bearing walls (partitions and enclosures). There are many advantages of using fired clay brick as the fire protection, the reduction of coating thickness, the solution for thermal and acoustic insulation, the reducing of thermal conductivity, which results in lower heat losses through the masonry walls. Thus, leading to increased energy efficiency of buildings and save energy.

The quality of the brick depends on the composition of raw materials, production method, firing method and firing temperature. The firing process sinters the particles of clay together to form a bond which gives the bricks its characteristic strength and durability. The sintering process is achieved by heating silicon dioxide or quartz (SiO$_2$) which occurs naturally in clay and shale to high temperatures, causing it to melt. Upon cooling, the quartz forms a bond between adjacent clay or shale particles at the points of contact.

One of the most common issues for Gaza Strip and other regions is accumulation of unmanaged wastes and the used raw materials in the production of construction materials such as clay brick. Especially, accumulation of unmanaged wastes has great importance in Gaza Strip which can be considered as self-sufficient in regards of brick-making raw material sources. Hence, solid wastes are candidates for incorporation into building materials to improve their performance such as be more durable and more energy efficient, and sustainable building materials. One technique
used to reduce such wastes is by recycling, which is not only benefits the environment but also to the economy.

Different kinds of wastes have already been recycled in ceramic industry. Example includes wasted glass, which are readily incorporated as an alternative ceramic raw material or as a fluxing agent in stoneware, tiles, bricks and concrete.

In general, bottles including juice, soft drink and sauce bottles, glass jars and other containers are among the sources of waste glass materials in many areas all over the world. In Gaza Strip, the resources of waste glass are glass originating from reconstruction and rehabilitation processes, glass bottles, glass jars, glass containers, glass plates and cups, Mirrors, residual glass from windows industry, light globes, medical or laboratory glass, televisions (TV), personal computers (PC) and ceramic products.

2.2 Fired Clay Brick

Fired clay bricks are made from clay by burning it at high temperature. With their attractive appearances and superior properties such as high compressive strength and durability, excellent fire and weather resistance, good thermal and sound insulation. Fired clay brick can be conveniently held in one hand and it is slightly longer than twice its width. Bricks are available in various sizes. In the United State (US) the most commonly used brick is the (extruded) modular brick, which measures $7\frac{5}{8} \times 3\frac{5}{8} \times 2\frac{3}{4}$ inch. Its nominal dimensions are $8 \times 4 \times 2\frac{2}{3}$ inch. In the United Kingdom (UK) the standard brick size is 215×102.5×65 mm, shown in Figure (2.1).

![Figure (2.1): (a) US common size brick, (b) UK standard size brick (Emmitt & Gorse, 2014; Mehta et al., 2013).](image)
2.2.1 Past and present

The first masonry units were based on dried mud and were used for the first time around 8000 BC in Mesopotamia, an area bordered by the Tigris and Euphrates rivers stretching from Southeast Turkey, Northern Syria, and Iraq reaching the Arabic Gulf (Pacheco-Torgal, & Jalali, 2011).

Since 3000 BC, as humans started to settle, bricks appeared as an interesting product, resistant, easily workable and usable, meaning that people could effectively protect themselves against the elements such as rain or wind and predators. For many years, bricks were hand-molded and sun-dried giving them rather fragile properties, but around 2500 BC the first fired bricks are produced (Chabat, 1881). Specially, when the Roman civilization has constructed several buildings with fired clay bricks.

The compressive strength and durability to weathering of fired clay bricks have made them a widely used construction material for thousands of years. Common clay-fired bricks still serve as the base of recent and amazing buildings.

With the appearance of Portland cement in the twenty-first century, masonry concrete blocks emerged as an alternative to fired clay bricks, although the latter are still predominant to a large extent. For instance in the UK, concrete blocks represent only around 5% of the total masonry units production (Bingel & Bown, 2009). Still, masonry fired clay bricks are and will continue to be widely used construction materials around the world, even in highly developed countries. US demand for fired clay brick and concrete block products is projected to increase nearly 12% annually from a weak 2009 base to 12.4 billion units in 2014 (66% clay bricks and 37% concrete blocks) (Freedonia Group, 2010). This represents just a small proportion of the annual worldwide production.

2.2.2 Types of fired clay bricks

There are thousands of types of bricks that are named for their use, size, forming method, origin, quality, texture, and materials.

2.2.2.1 Categorized by manufacture method:

1. Extruded – made by being forced through an opening in a steel die, with a very consistent size and shape.
• Wire cut – cut to size after extrusion with a tensioned wire which may leave drag marks.

2. **Moulded** – shaped in moulds rather than being extruded.
   • Machine – moulded – clay is forced into moulds using pressure.
   • Handmade – clay is forced into moulds by a person.

3. **Dry-pressed** – similar to soft mud method, but starts with a much thicker clay mix and is compressed with great force.

### 2.2.2.2 Categorized by use:

1. **Facing brick** – Facing bricks are intended for use in both structural and nonstructural masonry, including veneer, where appearance is a requirement.

2. **Hollow brick** – Hollow bricks are used as either building or facing brick but have a greater void area. Most hollow brick are used as facing brick in anchored veneer. Hollow brick with very large cores are used in reinforced brickwork and contain steel reinforcement and grout.

3. **Common or Building brick** – Building bricks are intended for use in both structural and nonstructural brickwork where appearance is not a requirement. Building bricks are typically used as a backing material.

4. **Thin brick** – Thin veneer bricks have normal face dimensions but a reduced thickness. They are used in adhered veneer applications.

5. **Paving brick** – Paving bricks are intended for use as the wearing surface on clay paving systems. As such they are subject to pedestrian and light or heavy vehicular traffic.

Specialized use bricks:

6. **Chemically resistant** – bricks made with resistance to chemicals.
   • Acid brick – acid resistant bricks.

7. **Engineering** – a type of hard, dense, brick used where strength, low water porosity or acid (flue gas) resistance are needed. Further classified as type A and type B based on their compressive strength.

8. **Fire or refractory** – Refractory Bricks can withstand high and do not fuse as these are chemically and physically stable even at a very high temperature (highly heat-resistant bricks). These bricks are Fired at (1250-1400 °C).
- Clinker – a vitrified brick.
- Ceramic glazed – fire bricks with a decorative glazing.

2.2.3 Brick manufacturing

2.2.3.1 Raw materials

The raw materials used in the manufacturing process of fired clay masonry units are a mixture of natural clay, silt, and sand. The surface clays (recent sedimentary formations), Shales (clays that have been subjected to high pressures) and fire clay (mined at deeper levels) are commonly used in the production of fired clay units. Surface and fire clays have a different physical structure from shales but are similar in chemical composition. The two main constituents of all of these clays are the silica and alumina. Some minor components are iron and other metal oxides, which are particularly responsible for giving brick its red-brown color. White and light-colored bricks are made by using clay that is naturally deficient in metal oxides and removing whatever metal oxides are present in it. White bricks are generally more expensive than the normal (red-brown) bricks. The range of chemical component and mineralogical phases present in clay shown in Table (2.1).

**Table (2.1): Range of chemical component present in clay (Walter Lee Sheppard, 1986).**

<table>
<thead>
<tr>
<th>Property</th>
<th>Fireclay Brick</th>
</tr>
</thead>
<tbody>
<tr>
<td>Chemical composition, wt. %</td>
<td></td>
</tr>
<tr>
<td>SiO₂</td>
<td>56.8 – 68.6</td>
</tr>
<tr>
<td>Al₂O₃</td>
<td>22.9 – 38.7</td>
</tr>
<tr>
<td>Fe₂O₃</td>
<td>0.8 – 3.0</td>
</tr>
<tr>
<td>K₂O</td>
<td>1 – 3.2</td>
</tr>
<tr>
<td>TiO₂</td>
<td>1 – 2.8</td>
</tr>
<tr>
<td>MgO</td>
<td>0.1 – 1.2</td>
</tr>
<tr>
<td>Na₂O</td>
<td>0.2 – 0.5</td>
</tr>
<tr>
<td>CaO</td>
<td>0.01 – 0.8</td>
</tr>
<tr>
<td>Phases identified</td>
<td>Trace – major</td>
</tr>
<tr>
<td>Quartz</td>
<td></td>
</tr>
<tr>
<td>Mullite</td>
<td>Minor – major</td>
</tr>
<tr>
<td>Cristobalite</td>
<td>None – major</td>
</tr>
<tr>
<td>Hematite</td>
<td>None – trace</td>
</tr>
<tr>
<td>Rutile</td>
<td>None – trace</td>
</tr>
<tr>
<td>Amorphous</td>
<td>Minor – major</td>
</tr>
</tbody>
</table>
2.2.3.2 Manufacturing process

Although modern technology has substantially changed the details of brick manufacturing, it is conceptually simple and consists of the following six operations, shown in Figure (2.2).

![Diagram of Manufacturing Process](image)

**Figure (2.2):** Diagrammatic Representation of Manufacturing Process (Brick Industry Association TN9, 2006).

### 2.2.3.2.1 Mining clay from the ground and storage of raw materials

Clays are mined in open pits with power equipment. Then the clay mixtures are transported to plant storage areas (Figure 2.3). Continuous brick production regardless of weather conditions is ensured by storing sufficient quantities of raw materials required for many days of plant operation.

![Clay or Shale being crushed and transported](image)

**Figure (2.3):** Clay or Shale being crushed and transported to storage area (Brick Industry Association TN9, 2006).
2.2.3.2.2 Preparing raw materials
To break up large clay lumps and stones, the material is processed through size-reduction machines before mixing the raw material (clay, sand, other additive materials).

2.2.3.2.3 Forming wet clay into the desired brick shape (green bricks)
Mixing, the first step in the forming process, produces a homogeneous, plastic clay mass. Usually, this is achieved by adding water to the clay in a pug mill, a mixing chamber with one or more revolving shafts with blade extensions. After pugging, the plastic clay mass is ready for forming. There are three principal processes for forming brick: stiff-mud, soft-mud and dry-press.

**Stiff-Mud Process** - In the stiff-mud or extrusion process (Figure 2.4), water in the range of 10 to 15 percent is mixed into the clay to produce plasticity. After pugging, the mixed clay goes through a deairing chamber that maintains a vacuum of 375 to 725 mm of mercury. Deairing removes air holes and bubbles, giving the clay increased workability and plasticity, resulting in greater strength. Next, the clay is extruded through a die to produce a column of clay. As the clay column leaves the die, textures or surface coatings may be applied. An automatic cutter then slices through the clay column to create the individual brick (Figure 2.5). Cutter spacing's and die sizes must be carefully calculated to compensate for normal shrinkage that occurs during drying and firing.

**Soft-Mud Process** - The soft-mud or molded process is particularly suitable for clays containing too much water to be extruded by the stiff-mud process. Clays are mixed to contain 20 to 30 percent water and then formed into brick in molds. To prevent clay from sticking, the molds are lubricated with either sand or water to produce “sand-struck” or “water-struck” brick. Brick may be produced in this manner by machine or by hand.

**Dry-Press Process** - This process is particularly suited to clays of very low plasticity. Clay is mixed with a minimal amount of water (up to 10 percent), then pressed into steel molds under pressures from 3.4 to 10.3 MPa by hydraulic or compressed air rams.
2.2.3.2.4 Drying green bricks

Wet brick from molding or cutting machines contain 7 to 30 percent moisture, depending upon the forming method. Before the firing process begins, most of this water is evaporated in dryer chambers at temperatures ranging from about 38 ºC to 204 ºC. The extent of drying time, which varies with different clays, usually is between 24 to 48 hours. Although heat may be generated specifically for dryer chambers, it usually is supplied from the exhaust heat of kilns to maximize thermal efficiency. In all cases, heat and humidity must be carefully regulated to avoid cracking in the brick. Drying proses over time as in Figure (2.6).
2.2.3.2.5  Firing dried bricks in a kiln

2.2.3.2.5.1  Aims of firing

Firing is a key process in the manufacture of ceramic products, as it controls many important properties of the finished ware. These include mechanical strength, abrasion resistance, dimensional stability, resistance to water and chemicals, and fire resistance.

2.2.3.2.5.2  Firing process

Bricks are fired between 6 and 36 hours, depending upon kiln type and other variables, kiln is usually heated by natural gas or coal at a temperature higher than 900°C. The kiln used in modern brick manufacturing plants is a long tunnel kiln (Figure 2.7). The firing of the clay bricks intends to improve durability through sintering, which can be seen as the bonding mechanism of clay particles.

Firing may be divided into five general stages: 1) final drying (evaporating free water); 2) dehydration; 3) oxidation; 4) vitrification; and 5) flashing or reduction firing. All except flashing are associated with rising temperatures in the kiln. Although the actual temperatures will differ with clay or shale, final drying takes place at temperatures up to about 204 °C, dehydration from about 149 °C to 982 °C, oxidation from 538 °C to 982 °C and vitrification from 871 °C to 1316 °C.

**Figure (2.6):** Drying curve for brick. (ILO & UNIDO, n.d.)
The clay is fired at a fusing temperature between 871ºC to 1482ºC, depending on the type of clay. For building brick and face brick the temperature is controlled between 871ºC and 1200ºC, while the temperature ranges between 1315ºC and 1482ºC for fire brick.

The key to the firing process is to control the temperature in the kiln so that incipient fusion is complete, and partial vitrification occurs but viscous fusion is avoided.

The rate of temperature change must be carefully controlled and is dependent on the raw materials, as well as the size and coring of the brick being produced. Kilns are normally equipped with temperature sensors to control firing temperatures in the various stages. Near the end, the brick may be “flashed” to produce color variations.

After the temperature has peaked and is maintained for a prescribed time, the cooling process begins. Cooling time rarely exceeds 5 to 24 hours depending on kilns type. Cooling is an important stage in brick manufacturing because the rate of cooling has a direct effect on color.

![A typical tunnel kiln](image)

**Figure (2.7):** A typical tunnel kiln (Mehta et al., 2003).

### 2.2.3.2.5.3 Physico-chemical changes during firing

Raw materials used in ceramic bodies are usually complex mixtures of clay minerals, with other mineral matter such as quartz, feldspars, carbonates, gypsum, iron oxides and sometimes organic matter. Refractory products are also made from a wide range of non-clay minerals, together with specialized additives and binders (which may include some clays). When clay-based ceramic products are fired in a kiln, any residual moisture is driven off at temperatures of between 100 and 200 ºC. If organic
matter and iron pyrites are present, oxidation takes place at temperatures of between about 300 and 500 °C. Water combined within the structure of clay minerals (‘crystal water’) is usually released at temperatures of between 500 and 650 °C, whilst carbonates such as calcite and dolomite dissociate with the release of carbon dioxide in the temperature range 750 to 950 °C.

The most important changes relating to the development of ceramic properties involve the breakdown of the lattice structure of the original clay minerals, followed by the formation of new crystalline compounds and glassy phases. The temperature at which vitrification (glass formation) takes place, varies according to the mineralogy of the clay. Vitrification usually commences at about 900°C and is completed by about 1050°C (for many brick clays) or about 1100°C in the case of more refractory fireclays. During the vitrification stage of ceramic firing, many non-clay minerals such as quartz, oxides or iron, lime compounds and alkalis (oxides of sodium and potassium) become incorporated in the fired body. Some sintering and solid solution occurs, and eutectic reactions take place at the interface of mineral grains and melt phases. Non-clay products such as some refractory products also depend on sintering, vitrification or recrystallization stages, but in most cases much higher temperatures are required to achieve the desired properties. (Mehta et al., 2003; Brick Industry Association TNT9, 2006; Amrhein & Porter, 2009)

### 2.2.3.2.6 Storing finished products

After fired bricks are removed from the kiln, sorted, strapped in cubes, and stored in the yard until delivery to the construction site, Figure (2.8).

![Figure (2.8): A typical storage yard at a brick manufacturing plant (Mehta et al., 2003).](image-url)
2.2.4 Properties of fired clay bricks

All properties of brick are affected by raw material composition and the manufacturing process. Most manufacturers blend different clays to achieve the desired properties of the raw materials and of the fired brick. This improves the overall quality of the finished product. The quality control during the manufacturing process permits the manufacturer to limit variations due to processing and to produce a more uniform product.

The most important properties of brick are 1) durability, 2) color, 3) texture, 4) size variation, 5) compressive strength and 6) absorption.

2.2.4.1 Durability

The durability of brick depends upon achieving incipient fusion and partial vitrification during firing. Because compressive strength and absorption values are also related to the firing temperatures, these properties, together with saturation coefficient, are currently taken as predictors of durability in brick specifications. However, because of differences in raw materials and manufacturing methods, a single set of values of compressive strength and absorption will not reliably indicate the degree of firing.

2.2.4.2 Color

The color of fired clay depends upon its chemical and mineral content of the raw materials, the firing temperatures, the method of firing control, and the atmosphere in the kiln. Of all the oxides commonly found in clays, iron probably has the greatest effect on color. Regardless of its natural color, clay containing iron in practically any form will exhibit a shade of red when exposed to an oxidizing fire because of the formation of ferrous oxide, white or yellow bricks have a higher lime content, as the temperature is increased the colour moves through dark red, purple and then to brown or grey at around 1300°C. When fired in a reducing atmosphere, the same clay will assume a dark (or black) hue. Creating a reducing atmosphere in the kiln is known as flashing or reduction firing.

Given the same raw material and manufacturing method, darker colors are associated with higher firing temperatures, lower absorption values and higher compressive
strength values. However, for products made from different raw materials, there is no direct relationship between strength and color or absorption and color.

2.2.4.3 Texture, coatings and glazes

Many brick have smooth or sand-finished textures produced by the dies or molds used in forming. A smooth texture, commonly referred to as a die skin, results from pressure exerted by the steel die as the clay passes through it in the extrusion process. Most extruded brick have the die skin removed and the surface further treated to produce other textures using devices that cut, scratch, roll, brush or otherwise roughen the surface as the clay column leaves the die (Figure 2.9). Brick may be tumbled before or after firing to achieve an antique appearance.

Although not produced by all manufacturers, glazed brick are made through a carefully controlled ceramic glazing procedure.

Figure (2.9): Brick textures are applied by passing under a roller after extrusion (Brick Industry Association TNT9, 2006).

2.2.4.4 Size variation

Clays shrink during both drying and firing; therefore, allowances must be made in the size of the finished product. Both drying shrinkage and firing shrinkage vary for different clays, usually falling within the following ranges:

- Drying Shrinkage 2 to 8 percent
- Firing Shrinkage 2.5 to 10 percent
Firing shrinkage increases with higher temperatures, which produce darker shades. When a wide range of colors is desired, some variation between the sizes of the dark and light units is inevitable.

To obtain products of uniform size, manufacturers control factors contributing to shrinkage. Because of normal variations in raw materials and temperature variations within kilns, absolute uniformity is impossible. Consequently, specifications for brick allow size variations.

2.2.4.5 Compressive strength and absorption

Both compressive strength and absorption are affected by properties of the clay, method of manufacture and degree of firing. For a given clay and method of manufacture, higher compressive strength values and lower absorption values are associated with higher firing temperatures. Although absorption and compressive strength can be controlled by manufacturing and firing methods, these properties depend largely upon the properties of the raw materials.

2.2.5 Specification for building brick

Current specification requirements for strength and absorption of building brick are given from ASTM C62, C216, C652 and listed in Table (2.2). Strength and absorption of brick from different producers vary widely.

Table (2.2): Physical requirements for various grades of building bricks (ASTM C67-03, 2003).

<table>
<thead>
<tr>
<th>Designation</th>
<th>Maximum Compressive Strength gross area, psi (MPa)</th>
<th>Maximum Water Absorption by 5-h Boiling, %</th>
<th>Maximum Saturation Coefficient $^A$</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Average of 5 Brick</td>
<td>Individual</td>
<td>Average of 5 Brick</td>
</tr>
<tr>
<td>Grade SW</td>
<td>3000 (20.7)</td>
<td>2500 (17.2)</td>
<td>17.0</td>
</tr>
<tr>
<td>Grade MW</td>
<td>2500 (17.2)</td>
<td>2200 (15.2)</td>
<td>22.0</td>
</tr>
<tr>
<td>Grade NW</td>
<td>1500 (10.3)</td>
<td>1250 (8.6)</td>
<td>No limit</td>
</tr>
</tbody>
</table>

$^A$ The saturation coefficient is the ratio of absorption by 24-h submersion in cold water to that after 5-h submersion in boiling water.
2.3 Glass

Glass has proven its importance in our lives through manufactured products such as sheet glass, bottles, glassware, and vacuum tubing (Park et al., 2004).

2.3.1 History

The glass industry is very ancient with records dating back to the Egyptians more than 3500 years ago. It is known that at least 6000 years ago-long before he had learned to smelt iron - man knew how to make glass.

The first glass furnaces were volcanoes, and the first man to use glass took it from the ground already fused and cooled. Natural glass formed by volcanic action is called obsidian and can be found in many parts of the world. It is usually black and translucent and was probably used to make arrow and spear heads, knives and razors.

The first man-made glass was in the form of a glaze - a mixture of sand and minerals heated and fused onto the surface of stone or ceramic objects in an oven, thus producing a hard, shiny outer layer.

By 1500 BC, man was forming glass beads and jewels and making small containers by dipping a sand core into molten glass. Glass threads applied while the glass was still hot gave the containers striking beauty.

Glass made before 100 BC was seldom transparent and it usually contained impurities and imperfections.

Until the 17th century, the only real advance was in the selection and purification of these ingredients. The pipe remained in use exclusively for producing all blown glass up to the 19th century and is still used for many types of modern glass working (Ward-Harvey, 2009).

After 1945, automated bottle production technology advanced continuously. The first electronically controlled machines were introduced in 1970.

Present day, glass plays an important role in everyday life, in research and science, in modern architecture and in future sectors. The glass industry is continuously discovering new applications for glass based on state of the art technology and recent scientific findings. One of the most recent applications for glass is its use as a
building material. Modern architectural designs feature expansive glass facades. Glass is also used as an insulating material in the form of glass fiber, it is used to make optical fibers for telephone calls or TV in communications technology and it makes a contribution to regenerative energy technology in PV systems. Glass is also a key component in displays and semi-conductors.

2.3.2 Raw materials and manufacture

The raw materials for glass manufacture are plentiful and fairly readily obtained by surface mining operations. They consist generally of sand (SiO₂), soda ash (Na₂CO₃), Limestone (CaCO₃), dolomite, feldspar, sodium sulphate. The major constituent - sand - supplies the silica which is the actual glass former.

The other minerals calcium oxide (CaO), magnesium oxide (MgO) and alumina (Al₂O₃) are added to provide for a better chemical durability and act as fluxes and refiners in the melting process. The raw materials are heated to approximately 1500°C to melt them and obtain chemical reaction. The glass is then cooled in controlled conditions, where it becomes viscous at 1000°C and hardens at about 500°C.

The viscous nature of hot glass allows it to be drawn, blown, spun, rolled or floated before hardening. The cooling process imparts to the glass a brilliant, hard and natural gloss. Reheating can change some characteristics.

Some other elements are introduced into glass to obtain special colorings and physical performance as in the heat-absorbing and heat-reflecting glass. These glass can be varied considerably in performance by very small quantities of metals, etc. as is the case with metal alloys.

Glass factories for flat sheet materials are now well equipped and staffed, with laboratories which maintain standards and quality controls of a very high level.

The older style factories now concentrate on the production of patterned glass for building where the ribbon of molten glass passes between two rollers, producing one smooth and one patterned surface.

The clear glass is almost exclusively produced by the modern ‘float glass’ factories.
Small artist/craftsman-type production units still exist for specialized artistic skills and glass uses. Figure 2.10 summarize the glass processing in Flow chart.

**Figure (2.10):** Flow chart of glass processing (Mukherjee, 2013).

### 2.3.3 Types of glass

Nearly all commercial glass fall into one of six basic categories or types. These categories are based on chemical composition. Within each type, except for fused silica, there are numerous distinct compositions (Corning Museum of Glass, 2011).

#### 2.3.3.1 Soda-lime glass

Soda-lime glass (Figure 2.11) is the most common (90% of glass made), and least expensive form of glass. Resistance to high temperatures and sudden changes of temperature are not good and resistance to corrosive chemicals is only fair. *Soda-lime glass is used to make windows, bottles, light bulbs and jars.* Soda-lime glass is light permeable and has a smooth, fine-pored surface, making it easy to clean. Soda-lime glass expands very quickly under the influence of heat so care should always be taken when putting hot water into a soda-lime glass container. Table (2.3) is a list of some of approximate compositions of soda-lime-silica glass.
Table (2.3): Approximate compositions of Soda-Lime-Silica glass (Shelby, 2005).

<table>
<thead>
<tr>
<th>Type of Glass</th>
<th>Composition (by weight)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Soda-Lime-Silica</td>
<td>73% Silica – 14% Soda – 9% Lime – 4% Magnesia – 0.1% Alumina</td>
</tr>
</tbody>
</table>

Figure (2.11): Soda-Lime-Silica glass.

2.3.3.2 Lead (Crystal) glass

Lead glass (Figure 2.12) has a high percentage of lead oxide (at least 20% of the batch). It is relatively soft, and its refractive index gives a brilliance that may be exploited by cutting. It is somewhat more expensive than soda-lime glass and is favored for electrical applications because of its excellent electrical insulating properties. Thermometer tubing and art glass are also made from lead-alkali glass, commonly called lead glass. This glass will not withstand high temperatures or sudden changes in temperature. lead glass is used as Lead Crystal Tableware. Table (2.4) is a list of some of approximate compositions of lead glass

Table (2.4): Approximate compositions of lead glass (Shelby, 2005).

<table>
<thead>
<tr>
<th>Type of Glass</th>
<th>Composition (by weight)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Lead (Crystal)</td>
<td>57% Silica – 31% Lead Oxide – 12% Potassium Oxide</td>
</tr>
</tbody>
</table>
Figure (2.12): Lead (Crystal) glass.

2.3.3.3 Boro-Silicate glass (Pyrex)

Glass with this composition is highly resistant to chemicals and temperature fluctuation. That’s why it is mainly used for chemical production applications, in laboratories, for ampoules and bottles containing pharmaceuticals (Figure 2.13), to package injectable, or as extremely durable lamp covers. Borosilicate glass is also used in the household for baking and soufflé dishes and other "heatproof" kitchenware. Table (2.5) is a list of some of approximate compositions of Boro-Silicate glass.

Table (2.5): Approximate compositions of Boro-Silicate glass (Shelby, 2005).

<table>
<thead>
<tr>
<th>Type of Glass</th>
<th>Composition (by weight)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Boro-Silicate</td>
<td>81% Silica – 13% Boron Oxide – 4% Soda – 2% Alumina.</td>
</tr>
</tbody>
</table>

Figure (2.13): Boro-Silicate glass (Company of IndiaMART InterMESH Ltd, n.d.).
2.3.3.4 **Aluminosilicate glass**

Aluminosilicate glass has aluminum oxide in its composition. It is able to withstand high temperatures and thermal shock and is typically used in combustion tubes, gauge glass for high-pressure steam boilers, and in halogen-tungsten lamps (Figure 2.14) capable of operating at temperature as high as 750°C (British Glass Manufacturers Confederation, 2013). Table (2.6) is a list of some of approximate compositions of Alumino-Silicate glass.

**Table (2.6):** Approximate compositions of Alumino-Silicate glass (Shelby, 2005).

<table>
<thead>
<tr>
<th>Type of Glass</th>
<th>Composition (by weight)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Alumino-Silicate</td>
<td>64.5% Silica – 24.5% Alumina – 10.5% Magnesia – 0.5% Soda</td>
</tr>
</tbody>
</table>

**Figure (2.14):** Alumino-Silicate glass

2.3.3.5 **Ninety-six percent silica glass**

Ninety-six percent silica glass is a borosilicate glass, melted and formed by conventional means, then processed to remove almost all the non-silicate elements from the piece. By reheating to 1200°C the resulting pores are consolidated. This glass is resistant to heat shock up to 900°C.

2.3.3.6 **Fused silica glass**

Fused silica glass is pure silicon dioxide in the non-crystalline state. It is very difficult to fabricate, so it is the most expensive of all glass. It can sustain operating temperatures up to 1200°C for short periods.
2.3.4 Glass recycling

Recycling of glass is a process to convert waste material to useful products. Theoretically, glass is a fully recyclable and can be recycled endlessly. Glass materials can be recycled endlessly without loss in quality, but in order to keep producing the best end product, the recycled materials must be of a high quality. Therefore, continuous residual amounts of waste glass resulting from construction deteriorations, domestic and medical disposals, and industrial output junk materials are still cumulating and hence need to be land filled or reused.

There are certain steps to recycle waste glass: 1) collection 2) sorting 3) Producing glass cullet 4) Removing contaminants and drying to get pure glass 5) end markets for recycled glass.

Worldwide there are many examples of successful recycling of waste glass: as a cullet in glass production, as raw material for the production of abrasives, in sand-blasting, as a pozzolanic additive, in road beds, pavement and parking lots, as raw materials to produce glass pellets or beads used in reflective paint for highways, to produce fiberglass, and as fractionators for lighting matches and firing ammunition (Park et al., 2004).

Recent researches made it possible to use waste glass in concrete as a replacement of aggregate, either in commodity products, with the only objective to utilize as much glass as possible, or in value added products that make full use of the physical and esthetic properties of color sorted crushed glass. Park et al. (2004) showed the advantages to have the mixing ratio of the crushed waste glass aggregate about 30%.
Many countries have been taking much effort to recycle waste glass bottles. A bottle recovery system has already been established, through which empty bottles previously containing refreshing beverages, condiments, milk, etc. are collected, washed, and reused. In addition, broken bottles and bottles previously containing chemicals, cosmetics, etc. are melted to be reused or crushed and turned into paving material, masonry unit material, glass marble, glass tile, glass fiber, lightweight blowing agents, etc. (Park, 2000; Glass Bottle Recycling Council, 1994; Clean Japan Center, 1997). In Korea, empty used bottles are similarly reutilized in that they are collected, sorted, and crushed to be used mostly as a raw material for new bottles. The UK currently recycles around 50% of container glass (like bottles and jars), while both Switzerland and Finland recycle more than 90% of their glass (Scrapnews, 2016). However, only negligible proportions of the total used bottles are actually currently being recycled.

US consumes about 12 million tons of glass and recycles about 25% only. For Turkey, this amount approaches 120,000 ton, 67% recycles, and it has been reported that in Germany 3 million ton of waste glass are being recycled (Topcu, & Canbaz, 2004). Generally, In 1998, an estimated 11 million t of glass entered the waste steam but only 29% of this material was recycled (USEPA, 2000). In other words, 7.8 million tons went into landfills, seemingly defeating the purpose of curbside collection and the investments of environmental agencies to improve recycling on the collection end. Unluckily, there is no glass recycling so far in Gaza Strip. Therefore, there is a potential to partially replace the waste glass powdered as a partial replacement for clay to produced fired clay bricks.

2.4 Previous Studies

Previous works have been reported that waste glass can be used as a potential fluxing agent to help lowering firing temperatures of clay bodies. The utilization of wasted glass could then be an alternative way to save energy in the production process and to reduce the manufacturing cost. In addition, waste glass, when incorporated into a mixture, could induce the vitrification in clay bodies, resulting in higher density, less water absorption, and lower drying shrinkage.
The idea of using glass as a brick flux (additive) has been researched and reported on for many years. In a sense, one could say that the concept goes back hundreds of years. In the competition to replicate Asian porcelain, early researchers added glass frit to clay formulas to attain translucence and density. Some formulas for Irish Belleek pottery claim that it was 50 percent glass frit (Peterson, 1996). The Italian Medici porcelains of the 16th century also contained large amounts of glass (Rado, 1988).

On a more pragmatic level, after the energy crisis of the early 1970’s, the United States Bureau of Mines sponsored research to see whether energy could be saved using ground glass as a brick flux (Tyrell et al., 1972). In the 1990’s the Clean Washington Center sponsored research on the viability of glass in clay bodies as a strategy to improve recycled glass markets (CWC Report GL99-1, 1999). The government of the United Kingdom sponsored studies and trials to investigate glass as a brick flux, both to save energy and to improve markets for recycled glass (Waste & Resources Action Programme Project, 2004). Recently, several researches around the world have been carried out summarizing the use of waste glass as additives for fired clay brick, tile and stoneware to enhance its properties. The waste glass can be mixed with clay in different proportions to prepare high quality bricks. The addition of waste glass to brick specimen range from 0.5 to 94% by mass, most studied tended to concentrate on range between 5% and 20% of glass by mass, with the glass particle size ranging from 45 to 600 µm. In all reported test results, shrinkage was found to increase as percentage glass by mass increased, as well as with increased firing temperature (Brown and Mackenzie, 1982; Sanders, 1998; Smith, 2004; Matteucci et al., 2002; Tucci et al., 2004; Chidiac and Federico, 2007; Hwang et al., 2006; Lin, 2007a; Lin, 2007; Luz and Ribeiro, 2007; Raimondo et al., 2007; Demir, 2009; Loryuenyong et al., 2009; Mustafi et al., 2011; Phonphuak et al., 2015). Hwang et al. (2006) also indicated that the finer glass (5 µm) exhibited twice the shrinkage of the coarse glass (150 µm) in compositions. While a glass particle size of less than similar to those of a control brick, the addition of course glass, with particle size range between 132 and 150 µm at 4% mass caused shrinkage to decrease (Sanders, 1998). According to the National Brick Research Council (NBRA, 2003),
larger particle sizes lead to incomplete sintering, where glass particles act more as an aggregate with sintered edges than a completely sintered medium.

In previous studies, the strength properties of specimens containing waste glass were determined by both compressive strength and modulus of rupture testing. The range of compressive strength values varied between specimens, which may be attributed to slight variations in particle size, specimen size, and firing temperature for each testing method. However, the trend for all results clearly indicates an increase in compressive strength with increased addition of waste glass, especially between 10% and 30% mass. (Shutt et al., 1972; Youssef et al., 1998; Leshina and Pavnev, 2002; Smith, 2004; Kim et al., 2005; Tucci et al., 2004; Chidiac and Federico, 2007; Lin 2007a; Demir, 2009; Loryuenyong et al., 2009; Phonphuak et al., 2015). Demir (2009) also observed that the amorphous nature of waste glass particles enhances the sintering action, which leads to achieving a better strength in bricks. Fired clay bricks with suitable mechanical properties can be obtained at a proper firing temperature by using waste glass with a content in the range of 15 to 30% by weight of clay (Loryuenyong et al., 2009). Moreover, (Phonphuak et al., 2015) stated that the use of 10 wt.% waste glass and firing at 900°C yielded bricks with similar strength compared to that of normal clay brick fired at 1000°C. In other research, Chidiac and Federico (2007) indicated that the strength and transport properties of clay bricks were found to improve as a result of the improvement of pore structure when 15% (by weight of clay) of both fine and coarse waste glass was added, the compressive strengths achieved in this research were much higher than those discussed in the literature (Shutt et al., 1972; Smith, 2004; Lin, 2007b). The general trends reported by both Shutt et al. (1972) and Lin (2007b) at 20% to 30% waste glass addition were recreated in this study with only 15% waste glass addition. This is most likely due to the use of smaller waste glass particle sized specimens than those tested in the literature. Leshina and Pavnev (2002) concluded that the optimum content of glass in a ceramic mixture is 15–20%, which makes it possible to produce ceramic wall materials meeting the requirements of the state standards regarding water absorption with improved mechanical properties. Also they observed A jump-like increase in compression strength in samples containing glass power with particle size of 140 – 315 µm. Moreover, when the clay tiles mixed with 70% of glass and fired at 1050°C,
the compressive strength in the tiles is about 210 MPa (Kim et al., 2005). Values reported for modulus of rupture demonstrate a similar trend, i.e., an increase in modulus of rupture with increased percentage of glass by mass (Shutt et al., 1972; Brown and Mackenzie, 1982; Sander, 1998; Matteucci et al., 2002; Lin, 2007; Luz and Ribeiro, 2007; Raimondo et al., 2007; Dondi, 2009; Mustafi et al., 2011). Brown and Mackenzie 1982 also studied the influence of particle size, plasticity and pressing pressure on the properties of a ceramic-like body containing 90% recycled waste glass. The result shown that a progressive increase in the proportion of fines in the sample results in a progressive increase in the degree of sintering, as reflected in increased strength. The course particle sizes lead to a marked deterioration in mechanical properties. Also the properties deteriorate progressively with increasing water content in clay. The effect of varying the pressing pressure is not large.

On the other hand and Besides firing shrinkage and mechanical properties, water absorption (WA) and apparent porosity (AP) properties of fired clay bricks containing waste glass were determined in previous studies. In all reported test results, both WA and AP were found to decrease as percentage glass by mass increased, as well as with increased firing temperature (Brown and Mackenzie, 1982; Youssef et al., 1998; Leshina and Pavnev, 2002; Matteucci et al., 2002; Kim et al., 2005; Hwang et al., 2006; Lin, 2007a; Lin, 2007; Luz and Ribeiro, 2007; Raimondo et al., 2007; Demir, 2009; Loryuenyong et al., 2009; Mustafi et al., 2011; Lin et al., 2013; Phonphuak et al., 2015). Loryuenyong et al., (2009) also indicated that water absorption as low as (2-3) % was achieved for bricks containing (15–30) % by weight of glass content and fired at 1100°C. When the glass waste content was 45 % by weight, apparent porosity and water absorption was rapidly increased. A preliminary experiment from the same author showed that with smaller particle size of glass, this problem can be avoided. Youssef et al. (1998) recommended to addition of glass at a level of 33.3 % by weight and firing at 1100°C to get 5.6 % water absorption for non-glazed floor tiles. Kim et al. (2005) indicated that the optimal properties obtained in the tiles are the water absorption of about 0.9%, and the apparent porosity of about 2.1%. when the composition containing the glass of 70% is fired at 1050°C. But Luz and Ribeiro (2007) who used glass particles size below 40 μm, reached the water absorption values of the tiles approximately to 0.0% by
using 20% waste glass content and 1150°C firing temperature. The SEM micrographs was used in the experimental tests, it showed that the increased glass phase and reduced porosity with waste glass addition (Phonphuak et al., 2015).

Moreover, WA was compared with standards by many authors (Youssef et al., 1998; Leshina and Pavnev, 2002; Lin et al., 2013). Lin et al. (2013) reported that the 24-h absorption rate of the waste glass brick made from samples containing 30% waste glass sintered at 1000°C all met the Chinese National Standard (CNS) building requirements for first-class brick (water absorption of the bricks were was 10% of the brick).

There is a lack of the comparable data available with respect to the durability testing of brick with waste glass additives. When water infiltrates into the brick, it decreases the durability (Demir, 2009). Results of the absorption coefficient testing, which is often a means of estimating durability, suggested an increase in durability with increasing waste glass addition (Shutt et al., 1972; Sander, 1998; Leshina and Pavnev, 2002; Smith, 2004; Chidiac and Federico, 2007; Demir, 2009; Lin et al., 2013). Leshina, and Pavnev (2002) who used sodium sulphate to simulate freeze-thaw (F/T) testing, reported that specimens containing 5% waste glass were resistant to at least 70 cycles of freezing and thawing. Lin et al. 2013 also indicated that the salt crystallization test and wet–dry tests showed that the addition of waste glass had highly beneficial effects in that it increased the durability of the bricks.

Different types of glass were incorporated in fired clay bricks and tiles in the literature. The ground waste glass was incorporated to the clay body by Phonphuak et al. (2015), Youssef et al. (1998), and Demir (2009). Loryuenyong et al. (2009) investigated the reuse of waste glass from structural glass walls in fired clay bricks. Leshina and Pavnev (2002) and Matteucci et al. (2002) used container glass cullet and Mustafi et al. (2011) used waste broken bottles for their works. Another type of waste glass was used by Lin et al. (2013), he studied the effect of solar panel waste glass on fired clay bricks. Moreover, Chidiac and Federico (2007) investigated the effect of non-recycled waste glass additives on fired clay brick. However, Hwang et al. (2006) concluded that there was no major difference between window glass and post-consumer glass being utilized in clay products. Other types of glass addition to
ceramics has also contributed to enhance their properties. The hazardous waste glass is one of this, it was used with fired clay bricks and tiles in previous studies. Dondi et al. (2009) investigated the utilization of funnel and panel glass of TV and PC glass waste mixed with clay. These systems comprised of waste glass with high Pb (funnel) or Ba–Sr concentrations (panel). It was demonstrated that adding of 2% of glass waste to clay body doesn’t bring about significant changes in the technological performance of fired bricks. But, adding more than 5% of the waste may have deleterious on mechanical properties and efflorescence. The results in this research for leaching test demonstrated no significant environmental pollutant emission. In other research, the utilization of wastes glass from thin film transistor-liquid crystal display (TFT-LCD) optical waste glass (TVs and computers) mixed with clay by Lin (2007a) and Lin (2007b), these wastes are composed mostly of glass with some heavy metals. TFT-LCD can be pulverized and ground and subsequently blended with clay. The advantages of less water absorption, less weight loss on ignition, and a gain in compressive strength in the clay-TFT-LCD waste glass bricks should encourage the use of TFT-LCD waste glass as a brick additive (Lin, 2007a). In another study, Raimondo et al. (2007) results showed that TV/PC cathodic tube and screen glass, added to a typical porcelain stoneware body, are able to partially replace the conventional industrial fluxes, without significant repercussions on the technological process. Their presence allow to obtain good technological and mechanical properties, complying with the latest requirements of the industrial practice. Moreover, both glass are able to modify the body sintering pattern with a different effectiveness degree.

2.5 Concluding Remarks

The previous studies showed that lots of efforts have been done for investigating the effect of using waste glass materials as an additive in the fired clay brick, but all of them are trying to conform to the relevant specifications in their local areas. This research aims to implement a similar task but with applying the available local materials.
Chapter (3)

Experimental Program
Chapter (3)

Experimental Program

3.1 Introduction

The experimental program for this research study is primarily concerned with investigating the potential usefulness of using waste glass in making fired clay bricks. Currently, the waste glass generated in Gaza Strip is thrown away into the dump areas. Waste glass usually is produced from empty glass containers and different construction and reconstruction remains and waste materials. The waste glass is to be milled into powder. Then the powder glass is mixed with raw materials to make fired clay brick and then observing the effect of recycled powdered glass on the properties of fired clay brick.

The use of waste glass as a clay body additive is therefore attractive both environmentally and economically. Adding waste glass to bricks not only reduces the consumption of clay raw material, diverts waste from landfills, it also provides potential profit in tipping fees for manufacturers. In additions to mining, transportation, and storage costs, the firing process is an aspect of brick production which is energy intensive. By reducing the firing temperature by even a few degrees, while still maintaining brick strength and durability, the energy requirements of the firing process could be reduced.

The experimental program of the current research was carried out to explore the effects due to the use of waste glass and the firing behavior and physical mechanical properties following the testing procedure specifications of ASTM.

All materials used in this study are locally available. Clay is to be used in this investigation with (0%, 10%, 20%, 30%, and 40%) of waste glass powder as a partial replacement for clay.

Figure (3.1) shows the methodology for manufacturing porous clay bricks and Figure (3.2) summaries the testing program in the form of a flow chart.
Figure (3.1): Methodology for manufacturing clay bricks.

Figure (3.2): Flow chart for testing program.
3.2 Preparing of Raw Materials

Clay material used in this research was obtained by mixing three types of raw clay in equal parts from three areas in Gaza Strip (east Gaza, east khan Younis, Al Qarara) (Figure 3.3). The waste glass was obtained from a local shop glazing windows in Khanyounis (Figure 3.4 B). The raw materials were initially subjected to preparation such as drying, milling and sieving; prepared by powdering in a laboratory to particle size smaller than 600 μm for both clay and waste glass (Figure 3.4 C) for brick production. Another particle size (150 μm) of waste glass was prepared to compare with 600 μm (Figure 3.5). The liquid limit, plastic limit and plasticity index for the clay used are 38, 20 and 18. The particle size distribution test was carried out for both clay and waste glass by using sieve size analysis and hydrometer method. The results of the particle size analysis are shown in Figure (3.6).

Figure (3.3): Clay raw materials as collected from three areas.
Figure (3.4): a) Clay, b) Waste glass, c) Clay and Waste glass powdered, d) Fired clay brick.

Figure (3.5): Different waste glass particle size (150 µm and 600 µm).

Figure (3.6): Particle size distribution curve of the clay and waste glass powder.

3.3 Experimental Procedures

In order to obtain comparable results, 19 different groups of samples were prepared for the tests depending on the amount of waste glass added, heating temperature and particles size of waste glass. The mix proportions were prepared based on the dry weight of the materials. Mixture proportions were presented in Table (3.1).
Solid brick clay samples were produced using pilot laboratory procedures and equipment (Figure 3.7). The raw materials were mechanically mixed for 5 min to get a uniform consistency (Figure 3.8). After dry mixing, water about 8 wt.% of total weight was sprayed to the powder mixtures for the production of semi-dry molded brick samples. Test specimens with a dimension 215mm (L)×102.5mm (W)×65 mm(H) were produced in a laboratory type moulded (Figure 3.9). A hydraulic press was used to make bricks by compressed it with a pressure of 15 MPa. The shaped samples were dried under laboratory conditions (21°C) for 24 h (Figure 3.10) and then dried in an oven (Figure 3.11). Samples were dried in an oven maintained at 45°C for 6 h and then at 110°C for 24 h. The dried samples were fired at 900, 1000 and 1100°C in an electrical furnace at a heating rate of 2.5°C/min until 600°C, and then 5°C/min until 900°C, 1000°C and 1100°C (Figure 3.12). The time taken to reach the required temperature was about 5 h to 6 h and the specimens were kept at this temperature for 1 h to achieved strength. The samples were naturally cooled down in the furnace. Thus, sufficient samples could be produced from each of the series of samples to perform the experiments (Figure 3.13). A total of 114 brick samples were prepared to testing purpose (Figure 3.4 D).

**Table (3.1):** The brick mixtures prepared from the raw materials used.

<table>
<thead>
<tr>
<th>Temperature (°C)</th>
<th>Group name</th>
<th>Clay (wt.%</th>
<th>Waste Glass (wt.%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>900</td>
<td>A1</td>
<td>100</td>
<td>0</td>
</tr>
<tr>
<td></td>
<td>B1</td>
<td>90</td>
<td>10</td>
</tr>
<tr>
<td></td>
<td>C1</td>
<td>80</td>
<td>20</td>
</tr>
<tr>
<td></td>
<td>D1</td>
<td>70</td>
<td>30</td>
</tr>
<tr>
<td></td>
<td>E1</td>
<td>60</td>
<td>40</td>
</tr>
<tr>
<td>1000</td>
<td>A2</td>
<td>100</td>
<td>0</td>
</tr>
<tr>
<td></td>
<td>B2</td>
<td>90</td>
<td>10 (Coarse and fine glass)</td>
</tr>
<tr>
<td></td>
<td>C2</td>
<td>80</td>
<td>20 (Coarse and fine glass)</td>
</tr>
<tr>
<td></td>
<td>D2</td>
<td>70</td>
<td>30 (Coarse and fine glass)</td>
</tr>
<tr>
<td></td>
<td>E2</td>
<td>60</td>
<td>40 (Coarse and fine glass)</td>
</tr>
<tr>
<td>1100</td>
<td>A3</td>
<td>100</td>
<td>0</td>
</tr>
<tr>
<td></td>
<td>B3</td>
<td>90</td>
<td>10</td>
</tr>
<tr>
<td></td>
<td>C3</td>
<td>80</td>
<td>20</td>
</tr>
<tr>
<td></td>
<td>D3</td>
<td>70</td>
<td>30</td>
</tr>
<tr>
<td></td>
<td>E3</td>
<td>60</td>
<td>40</td>
</tr>
</tbody>
</table>
Figure (3.7): Laboratory containers filled by milled clay.

Figure (3.8): Electrical mixer.

Figure (3.9): Brick making Mould.
Figure (3.10): Drying brick samples under laboratory conditions.

Figure (3.11): Drying brick samples in an oven.

Figure (3.12): Firing brick sample in electrical furnace.

Figure (3.13): Fired clay bricks.
3.4 Testing Program

For the testing program, six brick samples are prepared for each group of the 19 groups that listed previously in Table (3.1). These sixes brick samples are divided into two categories, one to test compressive strength and another to tests water absorption, firing shrinkage, bulk density and apparent porosity. A total number of 285 testing data points were used after controlling the compiled testing cases from data quality and completeness points of views.

The reference testing bricks for comparison purposes were the sample with no waste glass content, sample A1, A2 and A3 according to firing temperature.

Tests were carried out on at least 3 bricks and the average value of the results was reported.

3.5 Testing Method for the Physical and Mechanical Properties

The brick samples then underwent series of tests including water absorption, bulk density, apparent porosity, firing shrinkage and compressive strength, to determine their quality in comparison with the ASTM Standards methods.

3.5.1 Physical properties

Several physical properties of the fired clay bricks can be determined: linear shrinkage, water absorption, apparent porosity, bulk density, apparent density, and loss on ignition. In this research, only the first four properties were considered.

3.5.1.1 Linear shrinkage

Linear shrinkage was obtained by measuring the length of the sample before and after drying or before and after firing, or even over the whole process using a caliper with a precision of ±0.01 mm, according to the standard ASTM C326 (ASTM C326-09, 2014). The firing linear shrinkage (before and after firing) expressed as a percentage and calculated according to the following formula is presented, as these results were more readily available.

\[
\text{Firing shrinkage(\%)} = \frac{L_{\text{dried}} - L_{\text{fired}}}{L_{\text{dried}}} \times 100
\]
Where $L_{\text{dried}}$ is the length of the oven-dried sample (mm) and $L_{\text{fired}}$ is the length of the fired sample (mm).

Firing shrinkage was determined by measuring the physical dimensions of the specimens before and after firing.

### 3.5.1.2 Bulk density, Water absorption and Apparent porosity

The bulk density, Water absorption, and apparent porosity were measured according to Archimedes method described in standard ASTM C373 (ASTM C373-88, 2006), which involves drying the test specimens to constant mass (D), boiling them in distilled water for 5 h and soaking them for an additional 24 h, at ambient temperature. Following impregnation, the mass (S) of each specimen while it was suspended in water, and its saturated mass (M), were determined.

#### 3.5.1.2.1 Apparent porosity

During drying and firing, the added particles burn leaving voids due to their breakdown, but also to gas emissions by decomposition of the matter (water, carbon dioxide). Noteworthy, there is no fixed maximal porosity for fired clay bricks.

Apparent porosity expresses, as a percent, the relationship of the volume of open pores of the specimen to its exterior volume. Calculate the apparent porosity as follows:

$$P(\%) = \frac{M - D}{V} \times 100$$

where $V$ (cm$^3$) is the exterior volume ($V = M - S$).

D: dried mass

M: saturated mass

S: suspended mass in water

#### 3.5.1.2.2 Water absorption

The creation of porosity leads to an increase in water absorption. The voids in the structure while immersed, are filled with water and, depending on the arrangement of the pores and the way they are linked together, this can penetrate the material more or less easily, with a preferential pathway. For water absorption, no standardized
maximum value exists. However, a very large absorption capacity could be detrimental for the final brick as it may affect the durability of the product and its resistance to natural conditions.

Water absorption expresses as a percent, the relationship of the mass of water absorbed to the mass of the dry specimen. Calculate the water absorption as follows:

\[ A = \frac{M - D}{D} \times 100 \]

D: dried mass
M: saturated mass

3.5.1.2.3 Bulk density

The bulk density and the apparent density change (not including porous).

bulk density, in grams per cubic centimeter, of a specimen is the quotient of its dry mass divided by the exterior volume, including pores. Calculate the bulk density as follows:

\[ B = \frac{D}{V} \times 100 \]

where \( V \) (cm\(^3\)) is the exterior volume \( V = M - S \).

D: dried mass
M: saturated mass
S: suspended mass in water

3.5.2 Mechanical properties

To ensure the engineering quality of a material, especially for building construction use, mechanical testing is the essential criteria. the compression or bending strength are represent for mechanical properties.

3.5.2.1 Compressive strength

The compressive strength was measured for brick samples according to ASTM C67 (ASTM C67-03, 2003).
3.5.2.1.1 Specimen Size.

ASTM C67 requires that the specimen be full height and width, and approximately one-half of a brick in length, plus or minus 1 inch (25 mm). However, if the testing machine being used is not capable of providing sufficient force to crush the approximate half-brick, a piece of brick having a length of one-quarter of the original full brick length may be used, so long as the total cross-sectional area is not less than 14 inch² (90 cm²), (Figure 3.14). The specimen size that used in this research is 102.5×100×65 mm.

![Figure 3.14: Compressive Strength Specimens. (Brick Industry Association TNT39, 2001).](image)

Although ASTM C67 does not specifically state the method in which the samples are to be obtained, it has been common practice to use pieces of brick which are left over from sawing the units to the desired size is acceptable (Figure 3.15). A minimum of five specimens is required.
Figure (3.15): Saw machine.

The compressive strength test specimens should be oven-dried. The amount of moisture in the brick can affect its compressive strength; the higher the moisture content, the lower the apparent strength. Therefore, by drying the specimens before testing, one variable that can affect the results is eliminated.

3.5.2.1.2 Speed of Testing

The speed of testing specified in ASTM C67 should be adhered to, primarily for the purpose of obtaining consistent results. Past experience on the effect of the rate of loading on the compressive strength of specimens has shown that, as the rate increases, there can be significant increases in the apparent compressive strengths of the specimens. The requirements of ASTM C67, while not particularly specific, do provide a moderate rate of loading which, if followed, will produce consistent results that will represent more accurately the true compressive strengths of the specimens.

ASTM C67 specifies that the specimen should be loaded to one-half of the expected maximum load, and then the rate should be adjusted such that the test is completed in not less than one minute and not more than two minutes. For this reason, it is a good idea to do one or two preliminary tests to get an estimate of the maximum strength. Figure 3.16 illustrates the time vs. loading criteria of ASTM C67. The speed that used in this research is 2 KN/Sec.
3.5.2.1.3 Calculation and Reporting

The compressive strength is determined by dividing the maximum compressive load by the gross cross-sectional area of the specimen. Since five specimens are used, the arithmetic average should be determined. Calculate and compressive strength of each specimen to the nearest 0.01 MPa as follows:

\[
\text{Compressive strength} = \frac{W}{A}
\]

C = compressive strength of the specimen MPa,

W = maximum load, N, indicated by the testing machine, and

A = average of the gross areas of the upper and lower bearing surfaces of the specimen, mm².
Chapter (4)

Test Results and Discussion
Chapter (4)

Test Results and Discussion

4.1 Introduction

The bricks in this research were made from clay and waste glass by controlling the firing temperatures, waste glass ratio and particle size. At least 3 samples were used for each test for all groups listed previously in Table (3.1) and the averages are presented and discussed in this section. The investigated and reported physical and mechanical properties are bulk density, apparent porosity, water absorption, firing shrinkage and compressive strength are shown in the following.

4.2 Test Results

4.2.1 Firing shrinkage

Shrinkage is related to the loss of water among clay particles resulting in the closer packing of clay particles and resulted shrinkage. During firing, especially during sintering at high temperatures, ceramic particles fuse together leading to greater proximity and thus enhancing linear shrinkage. It is considered that the reduction in firing shrinkage of brick material had a positive impact. To minimize shrinkage, firing temperature which is an important parameter affecting the degree of shrinkage must be controlled during the firing process. Large shrinkage could create problems as it may cause cracks and dimensional defects. As shown in Table (4.1) and Figure (4.1), clay bricks were fired at temperatures between 900 and 1100°C. The firing shrinkage increased with increasing firing temperature and also increased with increasing the amount of waste glass. The addition of large amount of wasted glass decreased firing shrinkages of the bricks. Shrinkage is, normally, an important factor to determine the degree of densification during firing. From Figure (4.1), it can be seen that large amount of waste glass additive induces negative shrinkage, i.e. an expansion of the material. This evident in sample E3 which has 40 wt.% waste glass, the value of shrinkage in this case was equal to -5.20 (Figure 4.2). This may be due to appeared bubbles protruding from the exterior bricks and these bubbles have been formed due to a chemical reaction. Some bubbles that had been trapped in the
specimens caused expansion. This phenomenon typically occurs during sintering of materials containing small amounts of water. On the other hand, small amount of waste glass additives gives positive shrinkage, representing water evaporating out of the system. Bricks must have a firing linear shrinkage lower than 8% in order to retain good mechanical performance (Weng et al., 2003). The results showed that shrinkage occurred in the fired clay brick samples was in the range of 0.51 - 6.19%, whereas, the control fired clay bricks without any waste glass addition had comparable firing shrinkage between 0.51% - 1.03%. Shrinkage clearly depends on the amount of waste glass additive and the firing shrinkage. The firing shrinkage for all brick sample are within the safe limits for industrial production which indicated in ASTM C326. However, it can be seen that for all the additives tested, linear shrinkages are below 8%. In addition, the lower this result, the better the final product's properties.

**Table (4.1):** Average values of the firing shrinkage of the samples.

<table>
<thead>
<tr>
<th>Waste glass (%)</th>
<th>Firing shrinkage (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>900°C</td>
</tr>
<tr>
<td>0</td>
<td>0.51</td>
</tr>
<tr>
<td>10</td>
<td>0.69</td>
</tr>
<tr>
<td>20</td>
<td>0.71</td>
</tr>
<tr>
<td>30</td>
<td>0.78</td>
</tr>
<tr>
<td>40</td>
<td>0.81</td>
</tr>
</tbody>
</table>
Figure (4.1): Average values of the firing shrinkage of the samples.

Figure (4.2): Negative firing shrinkage fired clay brick with 40% waste glass and firing at 1100°C.

4.2.2 Bulk density

Density of fired clay brick depends on specific gravity of the raw material, method of manufacturing and degree of burning. As shown in Table (4.2) through Table (4.5) and Figure (4.3), Figure (4.5), Figure (4.6), and Figure (4.8), the density of fired clay brick increases, its strength also increases, while its water absorption and apparent porosity decreases. The bulk density of fired clay bricks was proportional to the firing temperature and the amount of waste glass added to the mixture. The result shows that the bulk density of fired clay brick sample without addition of waste glass that was reference brick (0G) at 1000°C was 1.81 g/cm³ while at 1100°C was 1.89 g/cm³, difference between the two values were about 0.08 g/cm³ which corresponds
to 4.1%. As the firing temperature increased, the bulk density increased. This is possible due to increased consolidation or vitrification between particles in the body with increasing of temperature. The bulk density of fired clay bricks also increased with an increase in the amount of waste glass. The bulk density of fired clay bricks fired at 900°C varied from 1.80 g/cm$^3$ to 1.82 g/cm$^3$, there is no marked effect. The effect is more pronounced for clay bricks fired at 1000°C, which were varied from 1.81 g/cm$^3$ to 1.87 g/cm$^3$, all show an improvement in bulk density that increases with an increase in the amount of waste glass. For firing temperature of 1100°C, the bulk density of fired clay bricks varied from 1.89 g/cm$^3$ to 1.97 g/cm$^3$, a slight increase is observed, then the bulk density tends to decrease to 1.64 g/cm$^3$ for more than 30% wt. waste glass addition. As a result, it could be deduced that the addition of waste glass at relatively low temperatures densifies the mixture. At higher temperatures, bloating presumably occurs having for effect to decrease the bulk density as the amount of waste glass grows larger. The bulk density is related to durability and water absorption of clay bricks. Figure (4.4) shows bulk density device.

**Table (4.2):** Average values of the bulk density of the samples.

<table>
<thead>
<tr>
<th>Waste glass %</th>
<th>Bulk density (g/cm$^3$)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>900°C</td>
</tr>
<tr>
<td>0</td>
<td>1.80</td>
</tr>
<tr>
<td>10</td>
<td>1.81</td>
</tr>
<tr>
<td>20</td>
<td>1.81</td>
</tr>
<tr>
<td>30</td>
<td>1.82</td>
</tr>
<tr>
<td>40</td>
<td>1.82</td>
</tr>
</tbody>
</table>
Figure (4.3): Average values of the bulk density of the samples.

Figure (4.4): Bulk density device.

4.2.3 Water absorption and apparent porosity

Water absorption is an important factor for the durability of clay bricks. When water infiltrates brick, it decreases the durability of brick. Thus, the internal structure of
brick must be sufficiently dense to void the leaking of water. To increase density and decrease water absorption of clay bricks, the firing temperature must be raised. Table (4.3), Table (4.4), Figure (4.5) and Figure (4.6), showed that the lowest water absorption value was obtained for fired clay bricks (E3) which has the lowest porosity. The highest water absorption value was seen in (A1) which has the highest porosity. As understood here, there is a close relationship between water absorption and apparent porosity of bricks. For clay brick samples fired at 900°C, the decreases in water absorption and apparent porosity are reasonable for small percentages additions, but nearly stops for waste glass in excess of 30%. For the other two temperatures 1000°C and 1100°C, the relation has almost a constant slope with a clear trend of much lower water absorption and apparent porosity with increasing percentages of waste glass. The reduction in both water absorption and apparent porosity after firing suggested the increase in the local liquid phase at high firing temperature, and thus contributed to a decrease in the pore volume. Generally, The water absorption values decreased with increasing firing temperature, and decreased with increasing amounts of waste glass in the mixtures. The water absorptions of clay bricks fired at the temperatures between 900 and 1100°C were in the range of 16.24% to 4.83%. Thus, The samples were found to be within ASTM C62 specifications (17% for Grade SW) (ASTM C62-04, 2004). The waste glass particles fused with the clay bodies and this contributed to the densification of the clay brick. Figure (4.7) shows water absorption test.

**Table (4.3):** Average values of the water absorption of the samples.

<table>
<thead>
<tr>
<th>Waste glass %</th>
<th>Water absorption (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>900°C</td>
</tr>
<tr>
<td>0</td>
<td>16.24</td>
</tr>
<tr>
<td>10</td>
<td>15.38</td>
</tr>
<tr>
<td>20</td>
<td>14.77</td>
</tr>
<tr>
<td>30</td>
<td>13.94</td>
</tr>
<tr>
<td>40</td>
<td>13.73</td>
</tr>
</tbody>
</table>
Figure (4.5): Average values of the water absorption of the samples.

Table (4.4): Average values of the apparent porosity of the samples.

<table>
<thead>
<tr>
<th>Waste glass %</th>
<th>Apparent porosity (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>900°C</td>
</tr>
<tr>
<td>0</td>
<td>33.67</td>
</tr>
<tr>
<td>10</td>
<td>30.76</td>
</tr>
<tr>
<td>20</td>
<td>29.41</td>
</tr>
<tr>
<td>30</td>
<td>27.6</td>
</tr>
<tr>
<td>40</td>
<td>27.83</td>
</tr>
</tbody>
</table>

Figure (4.6): Average values of the apparent porosity of the samples.
**Figure (4.7):** Water absorption test.

### 4.2.4 Compressive strength

The compressive strength is the most important index for assuring the engineering quality of a building material because with a higher compressive strength, other properties also improved. The results in Table (4.5) and Figure (4.8) indicated that the compressive strength of fired clay bricks depended greatly on the amount of waste glass addition and firing temperature. The addition of waste glass considerably contributed to vitrification and enhanced the strength development by closing the internal pores with glassy phase. There are three curves fitted for the data of compressive strength in MPa. For the samples fired at 900°C, the curve shows an initial increase in strength as waste glass is added. The value rises from 18.61 MPa to about 22.91 MPa as 10% waste glass is added. This is in accordance with Figure (4.5) where the value of apparent porosity drops to an almost constant value over 20% waste glass addition. This means that the increase in compressive strength at that low firing temperature is mainly due to reduction in porosity. At 1000°C there is a gradual increase in strength from 21.33 MPa (0% waste glass) to 43.17 MPa (40% waste glass addition) in harmony with the decrease in apparent porosity observed in Figure (4.6), although, as the amount of waste glass addition reaches 40%, there is a tendency for the compressive strength to reach a nearly fixed value. This may be due to the effect of the low strength of the glassy phase formed as its amount increases. This effect is more pronounced for the sample fired at 1100°C which reaches a peak in compressive strength at 30% waste glass addition followed by expanding the brick
samples and a serious decrease (Figure 4.2). In view of porosity results of Figure (4.6), it is clear that as the percentage glassy phase largely increases (at 1100°C), the reduction in apparent porosity does not play a marked role in sustaining high values of strength. The optimum compressive strength was 96.37 MPa, it obtained for the bricks containing 30 wt.% glass and fired at 1100°C. Figure (4.9) shows the fired clay brick after compression failure.

**Table (4.5):** Average values of the compressive strength of the samples.

<table>
<thead>
<tr>
<th>Waste glass %</th>
<th>900°C</th>
<th>1000°C</th>
<th>1100°C</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>18.61</td>
<td>21.33</td>
<td>28.82</td>
</tr>
<tr>
<td>10</td>
<td>22.91</td>
<td>30.67</td>
<td>47.45</td>
</tr>
<tr>
<td>20</td>
<td>20.41</td>
<td>32.34</td>
<td>77.75</td>
</tr>
<tr>
<td>30</td>
<td>21.91</td>
<td>42.75</td>
<td>96.37</td>
</tr>
<tr>
<td>40</td>
<td>17.88</td>
<td>43.17</td>
<td>55.98</td>
</tr>
</tbody>
</table>

**Figure (4.8):** Average values of the compressive strength of the samples.
Figure (4.9): Fired clay brick after failure in compression.

4.2.5 The effect of the glass particle size

Table (4.6) & Figure (4.10) show that a progressive increase in the proportion of fines in the sample results in a progressive increase in the degree of sintering, as reflected in increased strength, elasticity, density and shrinkage, and decreased apparent porosity. The result shows that the compressive strength of fired clay brick sample with addition of waste glass particle size smaller than 150 µm that was special reference brick (D2) at 1000°C was 65.81 MPa while reference brick (D2) was 43.17 MPa, difference between two values were about 22.64 MPa which corresponds to 52.4%.

Table (4.6): Compressive strength for bricks at different glass particle size.

<table>
<thead>
<tr>
<th>Waste glass %</th>
<th>Compressive Strength (MPa) @ 1000 °C</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Coarse glass (600 µm glass)</td>
</tr>
<tr>
<td>10</td>
<td>30.67</td>
</tr>
<tr>
<td>20</td>
<td>32.34</td>
</tr>
<tr>
<td>30</td>
<td>42.75</td>
</tr>
<tr>
<td>40</td>
<td>43.17</td>
</tr>
</tbody>
</table>
Figure (4.10): Compressive strength for bricks at different glass particle size.
Chapter (5)
Conclusions and Recommendations
Chapter (5)
Conclusions and Recommendations

5.1 Conclusions

Brick samples were heated to temperatures which varied between 900 and 1100°C for 6 h, with a heating rate of 2.5°C/min until 650°C, and then 5°C/min until 900°C, 1000°C and 1100°C. The conclusions derived from the aforementioned experiments are as follows.

1. The compressive strength of the fired clay bricks increased with increases in the amount of waste glass content and firing temperature.
2. The bulk density of the fired clay bricks increased with increases in the amount of waste glass content and firing temperature.
3. The firing shrinkage of the fired clay bricks increased with increases in the amount of waste glass content and firing temperature.
4. The apparent porosity of the fired clay bricks decreased with increases in the amount of waste glass content and firing temperature.
5. The water absorption of the fired clay bricks decreased with increases in the amount of waste glass content and firing temperature.
6. The strength of fired clay bricks is greatly dependent on the amount of waste glass and on the firing temperature.
7. The fired clay bricks are very porous if a significant amount of wasted glass is added (larger than 30 wt.% glass).
8. In this research the optimal heating temperature for maximum compressive strength and other properties is 1100°C.
9. The optimal amount of waste glass that can be mixed with clay to produce good quality bricks is 30% by weight.
10. The used ratio of waste glass in the brick body should not be more than 30% by weight.
11. There is a similar trend between compressive strength and bulk density.
12. The advantages of lower apparent porosity, lead to less water absorption and gain in compressive strength.
13. The particle size of waste glass powder is very important and has a significant
effect on the properties of fired clay brick; the finest the particle size, the
highest is the compressive strength.
14. Because fired clay bricks are indeed an economical product with cheap,
abundant raw materials, locally available, produced by a simple
manufacturing process (drying, firing) and their interesting physical and
mechanical, especially their strength and durability. It can be used as an
alternative to concrete blocks.
15. The advantages of using bricks as a masonry building units should stimulate
the use of waste glass as a brick additive in the near future.
16. When the amount of waste glass reaches 40% by weight, the brick samples
are expanded and lead to a marked deterioration in mechanical properties.
17. There is a close relationship between water absorption and apparent porosity
of fired clay bricks.

5.2 Recommendations For Further Research

The following recommendations are purposed for further research:

1. Study the performance of fired clay bricks under freezing and thawing
conditions.
2. Study the effect of waste glass additive on the thermal conductivity of fired
clay bricks.
3. Study the effect of firing time on the on the properties of fired clay bricks.
4. Field study is needed to show the social acceptance of using fired clay bricks as
alternative to concrete blocks.
5. The Ministry of Public Works and Housing, and The Engineers Syndicate are
to encourage using these bricks for constructing buildings, and to start with
the government buildings as pilot projects.
References
References


Work Team. (2009). *Pollution caused by solid waste, rubble, and construction debris is a serious threat to the sea and the shore of the Gaza Strip*. Palestine: Ocha.


Appendices
Appendix (A)
Research Photos

Figure (A.1): Dried clay.

Figure (A.2): Waste glass.
Figure (A.3): Milled clay with water content 8%.

Figure (A.4): Milled Clay and milled waste glass.

Figure (A.5): Liquid limit test.
Figure (A.6): Standard sieves.

Figure (A.7): Sieve analysis test.
Figure (A.8): Hydrometer test.

Figure (A.9): Drying clay bricks in the air conditions.
Figure (A.10): Drying clay bricks in the laboratory conditions.
Figure (A.11): Fired clay bricks.

Figure (A.12): Clay bricks fired at 1000C: (a) 0% glass, (b) 10% glass, c) 20% glass, d) 30% glass.
Figure (A.13): Fired clay Brick with 20% waste glass content.

Figure (A.14): Full and half fired clay brick.

Figure (A.15): Fired clay bricks for different types of clay.
Figure (A.16): Compression machine.
Figure (A.17): Milling waste glass by Loss Anglos machine.

Figure (A.18): Water absorption test.